BE IT KNOWN, that We, KENNETH D. HOPE, a citizen of the United States of America, and resident of Kingwood, County of Harris, State of Texas; MICHAEL S. DRIVER, a citizen of the United States of America, and resident of San Francisco, County of San Francisco, State of California; and THOMAS V. HARRIS, a citizen of the United States of America, and resident of Benicia, County of Solano, State of California, have invented new and useful improvements in

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8 HIGH VISCOSITY POLYALPHAOLEFINS 9 PREPARED WITH IONIC LIQUID CATALYST HIGH VISCOSITY POLYALPHAOLEFINS

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2 PREPARED WITH IONIC LIQUID CATALYST 3 FIELD OF THE INVENTION 4 The present invention relates to the preparation of high viscosity 5 polyalphaolefins prepared using an ionic liquid catalyst. 6 BACKGROUND OF THE INVENTION 7 Alphaolefins may be oligomerized to prepare synthetic lubricating oil base 8 stocks which have desirable lubricating properties such as a low pour point 9 and a high viscosity index (VI). However, very high viscosity polyalphaolefins. 10 such as disclosed in U.S. Patent 4.827.064, are expensive to manufacture 11 using conventional oligomerization processes. U.S. Patent 5.304.615 teaches 12 the oligomerization of butene using an ionic liquid catalyst. European Patent 13 Application 97300875.8 describes a process for oligomerizing alphaolefins. 14 such as decene, using an ionic liquid catalyst to produce polyalphaolefins 15 having a viscosity up to about 20 centistokes (cSt) at 100°C. Unfortunately, 16 the process taught in this application has not been shown to be suitable for 17 making very high viscosity material, i.e., polyalphaolefins having a viscosity 18 above 22 cSt at 100°C. 19 Additionally, the prior art teaches the use of imidazolium, pyridinium, or 20 phosphorium as one component in the ionic liquid in addition to aluminum

described in WO 95/21872 as being useful for olefinic oligomerization. 23 Applicants have found that it is possible to readily make polyalphaolefins 24 having very high viscosity using an ionic liquid catalyst by carrying out the 25 oligomerization reaction in the absence of organic solvents which have 26 hitherto been used as a diluent for the feed. Accordingly, Applicants have

halide or gallium halide. Ternary compositions with ammonium halides are

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- 1 been able to make polyalphaolefins from feeds comprised primarily of olefins,
- 2 such as decene and dodecene, having viscosities in excess of 22 cSt and
- 3 even in excess of 30 cSt. Polyalphaolefins made using the process of the
- 4 present invention also have been shown to display excellent viscosity index
- 5 (VI) values, low pour points, and low Noack volatility values.
- 6 As used in this disclosure, the words "comprises" or "comprising" is intended
- 7 as an open-ended transition meaning the inclusion of the named elements,
- 8 but not necessarily excluding other unnamed elements. The phrase "consists
- 9 essentially of" or "consisting essentially of" is intended to mean the exclusion
- 10 of other elements of any essential significance to the combination. The
- 11 phrase "consisting of" is intended as a transition meaning the exclusion of all
- 12 but the recited elements with the exception of only minor traces of impurities.

SUMMARY OF THE INVENTION

The present invention is directed to a process for producing a very high viscosity polyalphaolefin product comprising contacting a feed consisting essentially of at least one alphaolefin having from 4 to about 14 carbon atom with an effective oligomerizing amount of an acidic ionic liquid oligomerization catalyst, maintaining said feed and oligomerization catalyst under preselected oligomerization conditions for a sufficient time to oligomerize the alphaolefin to the polyalphaolefin product, and recovering the high viscosity polyalphaolefin product. As noted above, it has been found that very high viscosity products may be obtained using the process of the present invention by carrying out the oligomerization reaction in the absence of organic diluent. Using the process of the invention, polyalphaolefins having viscosities in excess of 22 cSt and even in excess of 30 cSt may be readily prepared. Especially preferred in preparing the polyalphaolefin product are feeds comprising decene or dodecene.

1 The acidic ionic liquid oligomerization catalyst usually will be comprised of at 2 least two components, and in most instances it will be a binary catalyst, i.e., it 3 will consist of only two components. The first component is a compound 4 selected from the group consisting of aluminum halide, alkyl aluminum halide. 5 gallium halide, and alkyl gallium halide. Preferred compounds for use as the 6 first component of the oligomerization catalyst are an aluminum halide or an 7 alkyl aluminum halide, such as, for example, aluminum trichloride. The 8 second component is quaternary ammonium, quaternary phosporium, or 9 tertiary sulfonium, such as, for example, a liquid salt selected from one or 10 more of hydrocarbyl substituted ammonium halides, hydocarbyl substituted 11 imidazolium halide, hydrocarbyl substituted pyridinium halide, alkylene 12 substituted pyridinium dihalide, or hydrocarbyl substituted phosphonium 13 halide. Particularly preferred as the second component are alkyl substituted 14 ammonium halides, such as trimethylamine hydrochloride or alkyl substituted 15 imidizolium halides, such as 1-ethyl-3-methyl-imidazolium chloride. The mole 16 ratio of the two components will usually fall within the range of from about 1:1 17 to about 5:1 of said first component to said second component, and more 18 preferably the mole ratio will be in the range of from about 1:1 to about 2:1.

The use of a binary catalyst composition consisting essentially of trimethylamine hydrochloride and aluminum trichloride is particularly advantageous for carrying out the process of the present invention due to the ease of preparation, the ready commercial availability of the components, and the relatively low cost.

The amount of catalyst present to promote the oligomerization of the
alphaolefin should be not less than an effective oligomerizing amount, that is
to say, the minimum amount of the catalyst necessary to olgomerize the
alphaolefin to the desired product. This may vary to some degree depending
on the composition of the catalyst, the ratio of the two components of the
catalyst to one another, the feed, the oligomerization conditions chosen, and
the like. However, a determination of the effective catalytic amount should be

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- 1 well within the ability of one skilled in the art with no more than routine testing
- 2 necessary to establish the amount needed to carry out the invention.
- 3 The present invention is also directed to the unique polyalphaolefin product
- 4 prepared using the present invention. This product is characterized by a
- 5 viscosity of not less than 22 cSt at 100°C, and more preferably will have a
- 6 viscosity of at least 30 cSt at 100°C. In addition, the polyalphaolefin product
- 7 will display a low pour point, preferably less than -30°C, and low volatility.
- 8 preferably with a Noack number of 3 or less. Preferably, the product will have
- 9 a dimer content of less than 2 weight percent.

DETAILED DESCRIPTION OF THE INVENTION

As noted above, it is essential that the oligomerization reaction be conducted in the absence of any organic diluent. In carrying out the process of the present invention, the alphaolefin feed may be added to the catalytic mixture or the catalyst may be added to the alphaolefin feed. In either case, the feed and the product formed during the oligomerization will form a separate phase from the ionic liquid which allows the two phases to be readily separated. In order to facilitate mixing of the catalyst and the feed, it is desirable to either stir the oligomerization mixture or bubble the alphaolefin feed through the ionic liquid catalyst. Following completion of the oligomerization reaction, the mixing should be halted, and the product and residual feed should be allowed to form a distinct layer apart from the catalyst phase. In previous processes, the feed and product phase usually also contained an organic diluent, such as hexane. Applicants have discovered the presence of the organic diluent of the previous processes interferes with the oligomerization reaction and prevents the formation of the desired very high viscosity polyalphaolefin product.

The feed will consist essentially of one or more alphaolefins having from 4 to about 14 carbon atoms in the molecule, generally from about 8 to about

1 12 carbon atoms. Especially preferred are feeds containing 1-decene and

2 1-dodecene. While the feed may consist of a mixture of different alphaolefins,

3 it is essential that the feed not contain any organic diluent. As explained

4 above and as further illustrated in the examples below, it has been found that

5 the presence of an organic diluent interferes with the oligomerization reaction

6 and prevents the formation of the desired very high viscosity polyalphaolefin

7 product. This differs from the prior processes which included an organic

8 diluent, such as hexane or heptane, as part of the organic phase of the

9 reaction mixture.

10 The acidic ionic liquid oligomerization catalyst is comprised of two

11 components which form a complex. The first component of the catalyst which

12 will usually comprise a compound selected from the group consisting of

13 aluminum halide, alkyl aluminum halide, gallium halide, and alkyl gallium

14 halide. Especially preferred for the first component are aluminum halide or

15 alkyl aluminum halide. Aluminum trichoride has been used successfully as

16 the first component for preparing the oligomerization catalyst used in

17 practicing the present invention.

18 The second component making up the catalyst is an ionic liquid which is

19 primarily salt or mixture of salts which melts below room temperature. Ionic

20 liquids may be characterized by the general formula Q⁺ A⁻, wherein Q⁺ is

21 quaternary ammonium, quaternary phosphonium, or quaternary sulfonium,

22 and A is a negatively charged ion such as Cl, Br, OCl, NO3, BF, BCl, BCl,

23 PF₆, SbF₆, AlCl₄, ArF₆, TaF₆, CuCl₂, FeCl₃, SO₃CF₃, SO₃C₇H₇, and

24 3-sulfurtrioxyphenyl. Preferred for use as the second component are those

25 quaternary ammonium halides containing one or more alkyl moieties having

26 from 1 to about 9 carbon atoms, such as, for example, trimethylamine

27 hydrochloride, or hydrocarbyl substituted imidazolium halides, such as, for

28 example, 1-ethyl-3-methyl-imidazolium chloride.

- 1 The presence of the first component should give the ionic liquid a Lewis (or
- 2 Franklin) acidic character. Generally, the greater the mole ratio of the first
- 3 component to the second component, the greater the acidity of the ionic liquid
- 4 mixture. When aluminum trichloride and trimethylamine hydrochoride are
- 5 used as the first and second components, respectively, of the acidic ionic
- 6 liquid oligomerization catalyst, they preferably will be present in a mole ratio of
- o inquid oligometization catalyst, they preferably will be present in a mole ratio of
- 7 from about 1:1 to about 2:1.
- ${\small 8} \quad \text{ The oligomerization reaction takes place over a wide temperature range, but }$
- 9 preferably is carried out at about ambient temperature or slightly below. The
- 10 oligomerization reaction is somewhat exothermic and it may be desirable to
- 11 control the reaction temperature with an aqueous guench. Preferably, the
- 12 temperature of the reaction mixture will be maintained below about 50°C and
- 13 most preferably will be maintained below about 30°C.
- 14 Following completion of the oligomerization reaction, the organic layer
- 15 containing the alphaolefin product and residual olefin feed is separated from
- 16 the ionic liquid phase. The unreacted olefin and dimers may be removed from
- 17 the product by conventional means, such as by distillation, and recycled back
- 18 for further conversion. Likewise, the acidic ionic liquid catalyst that remains
- 19 after recovery of the organic phase may be recycled to the oligomerization
- 20 zone.

- 21 Following recovery of the polyalphaolefin product, it is generally desirable to
- 22 hydrogenate the unsaturated double bonds which remain in the product
- 23 mixture. This is readily accomplished by conventional means well known to
- 24 those skilled in the art. The hydrogenation of the unsaturated bonds is usually

carried out with hydrogen in the presence of a hydrogenation catalyst such as.

- 26 for example, catalyst containing nickel, palladium, platinum, cobalt or the like.
- 27 The present invention may be further illustrated by the following example
- 28 which is not intended to be a limitation on the process.

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EXAMPLE 1

2	A catalyst mixture was prepared using a 2 to 1 ratio of aluminum trichloride to
3	trimethylamine hydrochloride. The catalyst (39.2 g) was placed in a 1 liter
4	round bottom flask to which 401.2 g of 1-decene was added dropwise. The
5	initial temperature of the oligomerization mixture was 0°C which was allowed
6	to raise to 22°C. An inert atmosphere was maintained by a nitrogen sweep
7	gas/bubbler. The reaction was allowed to proceed for 1 hour and was
8	quenched with aqueous potassium hydroxide. The product was water
9	washed and hydrogenated using a nickel catalyst. The residual monomer and
10	dimer were removed by distillation. The distilled oligomer was found to
11	display the following properties:

12	100°C Kinematic Viscosity	31.6 cSt
13	40°C Kinematic Viscosity	283 cSt
14	Viscosity Index	152
15	Pour Point	-39°C
16	Noack Volatility	1.68%

17 EXAMPLE 2

The general procedure was the same as in Example 1, above, except for the addition of 185 grams of heptane diluent which was mixed with 400 grams of decene. Catalyst was prepared in a 2 to 1 molar ratio of aluminum trichloride to trimethylamine hydrochloride and 40.1 grams were added to the reaction in a dropwise manner. The initial reaction temperature was -6°C. The product was water washed and hydrogenated using a nickel catalyst. The residual monomer and dimer were removed by distillation to less than 1%. The distilled oligomer was found to display the following properties:

26 100°C Kinematic Viscosity 15.0 cSt 27 40°C Kinematic Viscosity 109 cSt Viscosity Index
 Pour Point
 45°C

- 3 It should be noted that the kinematic viscosity of the oligomer of Example 2
- 4 was significantly less at both 100°C and 40°C than that for the oligomer of
- 5 Example 1. The viscosity index of the product of Example 2 was also lower.